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CONTROL AND SIMULATE OF LIQUID LIQUID EXTRACTION COLUMN

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Abstract—The control strategy was developed in which a cascade control system was constructed where the level is taken as a master loop and the extract composition as a secondary loop. The transfer functions were identified from the literature and characteristic equations were determined. The ultimate gains and periods were obtained, using the average between direct substitution, Root locus and Bode methods. The ultimate gains and periods were inserted in Ziegler tuning table and the optimum adjustable parameters (K_c , τ_i , τ_d) were taken for P,PI&PID. These were inserted into each overall transfer functions and the controller that gave minimum overshoot was taken and introduced into either loop, the controller was the secondary loop is P controller and for the primary loop is also P controller. It's recommended that the controller system obtained in this process is to be made into digital computer system where each controller is a PLC.

Keywords— strategy, cascade, transfer function, tuning

1. INTRODUCTION

Acetic acid is one of the most widely used carboxylic acids. It is used in many reactions, for example in synthesis of acetic esters, or it can be used as a solvent, for example in the manufacture of cellulose acetate or pharmaceutical products. Acetic acid biosynthesis produces important quantities of aqueous solutions from which acetic acid should be economically recovered [1-2].

The separation of acetic acid from aqueous solutions by simple rectification is difficult, requiring a column with many stages and a high reflux ratio, the whole process being very expensive. Other processes may be used, depending on the acetic acid concentration in the solution. For example, extractive distillation is used for acid concentrations between 50 and 70 % w/w. By adding a third component water volatility is increased and the process may be carried out with low energy consumption. For acetic acid concentrations lower than 40 % w/w the liquid- liquid extraction can be

an appropriate process. This process is also useful when other components interfere with direct distillation [3-4].

Until recently, however, the acid waste has been mostly subjected to neutralization without any proper treatment. However, the conventional neutralization treatment has problems of formation of precipitation in a large quantity, cost of alkali, sludge disposal and treatment of waste water to reduce BOD and COD, which consequently cause an increase in the treatment cost. On the other hand, in this era of recycling it is important to minimize the waste by possibly reusing several components of the waste. This is not only important from economical point of view but also from the environmental aspects.

In this paper the control strategy will be discussed for liquid-liquid extraction column, the control of these units can often be problematic, partially due to their multiphase nature, and partially due to the difficulty of on-line measurements of output variables. Thus, the reliable simulation of the transient behavior of these columns is extremely valuable. The column hydrodynamics including flooding, entrainment, weeping, and phase inversion will be controlled.

Controller stability:

The stability of a linear system is determined from the system characteristic equation. The controller stability methods are following:

Routh-Hurwitz Method

The Routh criterion determines the number of the roots of the characteristic equation that lie on the left-half plane, the right-half plane or on the imaginary axis if the system is stable, unstable or critically stable respectively.

The Root Locus Method

This method gives an approximate graphical representation of the root as the gain is varied. This is very useful in the design of a system since it gives the position of the poles of the system in the S-plane for all values of the gain [5 -6]



- The appropriate transfer functions were cited [11].
- The overall transfer functions were determined and the open loop and close loop characteristic equations were derived.
- The characteristic equations developed in the previous step were used for tuning, stability analysis and offset investigation.
- The response by each criterion were graphically determined and compared for the best performance with regard to overshoot, decay ratio, rise time and recovery time (Fig. 6,7,8 &9).

Top of the extraction column ,the secondary loop:

The inner loop (Secondary loop)

$$G(s) = \frac{\pi_f}{1+\pi_l}$$

$$\Pi_f = G_{c2} G_v G_{p2}$$

$$1 + \Pi_L = 1 + G_{c2} G_v G_{p2} G_{m2}$$

$$G(s) = \frac{G_{c2} G_v G_{p2}}{1 + G_{c2} G_v G_{p2} G_{m2}}$$

The characteristic equation of the inner loop:-

$$1 + G_{c2} G_v G_{p2} G_{m2} = 0$$

III RESULTS AND DISCUSSION

$$\pi_F = k_{c2} \cdot \frac{3}{0.2S + 1} \frac{1}{(3S + 1)(S + 1)}$$

$$\pi_l = \frac{1.5 k_{c2}}{(0.2S + 1)(3S + 1)(S + 1)}$$

The closed-loop transfer function:

$$\frac{3 k_{c2}}{(0.2S + 1)(3S + 1)(S + 1) + 1.5 k_{c2}}$$

The characteristic equation: $1 + \pi_L = 0$

$$1 + \frac{1.5 k_{c2}}{(0.2S + 1)(3S + 1)(S + 1)} = 0$$

$$(0.2S + 1)(3S + 1)(S + 1) + 1.5 K_{C2} = 0$$

$$0.6S^3 + 3.8S^2 + 4.2S + (1 + 1.5K_{C2}) = 0$$

To get the ultimate gain K_{C2} for the secondary loop:

1. Routh-Hurwitz method

Rows	Coefficients	
S^3	0.6	4.2
S^2	3.8	$1 + 1.5k_{c2}$
S^1	$4.04 - 0.237k_{c2}$	0
S^0	$1 + 1.5k_{c2}$	0

$$4.04 - 0.237 K_{C2} = 0$$

$$K_{C2} = 17.05$$

To get the ultimate period, P_u :

Let $3.8 S^2 + (1 + 1.5 K_{C2}) = 0$, and Set $s = i\omega$ and $i^2 = -1$

$$-3.8 \omega^2 + 1 + 1.5k_{c2} = 0$$

$$-3.8 \omega^2 + 1 + 1.5 \cdot 17.05 = 0$$

$$\omega = \sqrt{(25.575/3.8)} = 2.59 \text{ Rad/sec}$$

$$P_u = 2\pi/\omega = 2\pi/2.59 = 2.42 \text{ sec}$$

2. direct substitution method:

Set $s = i\omega$ and $i^2 = -1$, in the characteristic equation:

$$-0.6 i\omega^3 - 3.8 \omega^2 + 4.2 i\omega + 1 + 1.5k_{c2} = 0$$

Taking the imaginary part:

$$-0.6 i\omega^3 + 4.2 i\omega = 0$$

$$\omega = \sqrt{(4.2/0.6)} = 2.64 \text{ Rad/sec}$$

The ultimate period, P_u :

$$P_u = 2\pi/\omega = 2\pi/2.64 = 2.38 \text{ sec}$$

Taking the real part:

$$-3.8 \omega^2 + 1 + 1.5k_{c2} = 0$$

$$-3.8 \cdot 2.64^2 + 1 + 1.5 k_{c2} = 0$$

$$k_{c2} = 16.99$$

3. Root-locus method using MATLAB

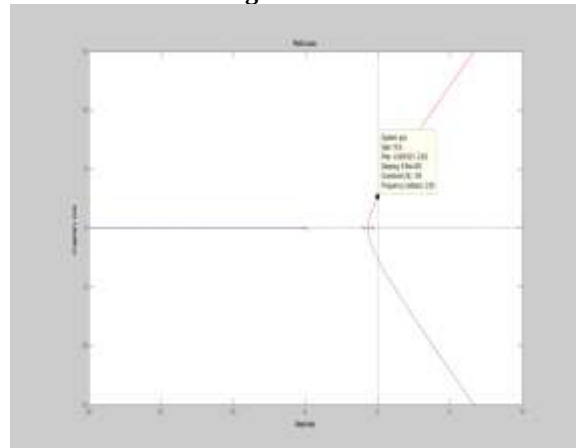


Fig 3: Root locus plot for the secondary loop using Matlab

From the figure: the system is stable since the root of the characteristic equation is not have positive real parts (i.e root locus plot does not cross the imaginary access)

$$k_{C2} = 16.8 \text{ and } \omega = 2.63 \text{ Rad/sec}$$

$$P_u = 2\pi/\omega = 2\pi/2.63 = 2.39 \text{ sec}$$

4. Bode plot method using Matlab for the secondary loop

$$\pi_F = k_{c2} \cdot \frac{3}{0.2s + 1} \frac{1}{(3s + 1)(s + 1)}$$

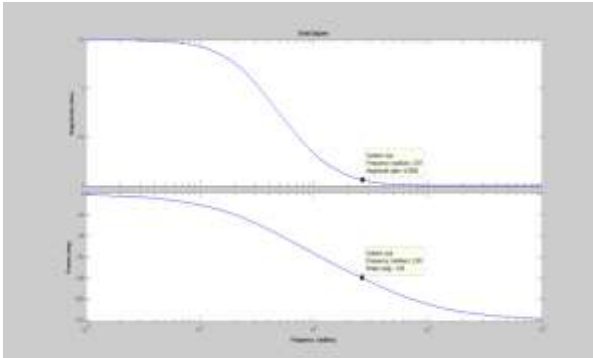


Fig4. bode plot for the secondary loop bottom level loop

From the figure: the system was stable up to -180C

$$P_u = 2\pi/\omega = 2\pi/2.65 = 2.38 \text{ sec}$$

$$AR = 0.0598$$

$$k_{c2} = 1/AR = 1/0.0598 = 16.72$$

The average of ultimate gains k_u and ultimate periods P_u

$$k_u \text{ average} = (k_{u1} + k_{u2} + k_{u3} + k_{u4})/4 = (17.05 + 16.99 + 16.8 + 16.72)/4 = 16.89$$

$$\text{And the } P_u \text{ average} = (P_{u1} + P_{u2} + P_{u3} + P_{u4})/4 = (2.42 + 2.38 + 2.39 + 2.38)/4 = 2.39$$

The primary loop

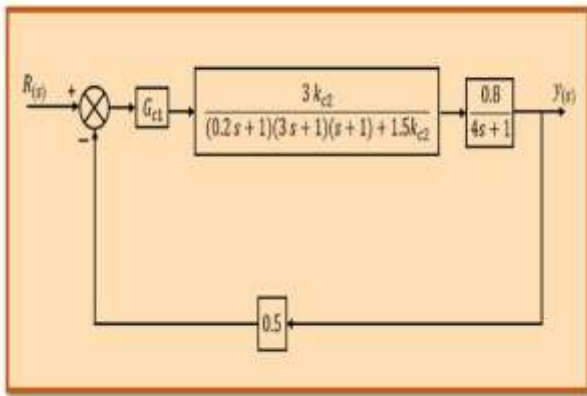


Fig 5: The reduced block diagram for the primary loop

With the same methods for the secondary loop, the primary loop

The average of ultimate gains k_u and ultimate periods P_u

$$k_u \text{ average} = (k_{u1} + k_{u2} + k_{u3})/3 = (7.15 + 7.2 + 7.09)/3 = 7.15$$

And the P_u average

$$= (P_{u1} + P_{u2} + P_{u3})/3 = (4.08 + 4.08 + 4.08)/3 = 4.08 \text{ sec}$$

Controller tuning: Using Z-N tuning controller for

- proportional controller: the adjustable parameters $k_{c1} = 0.5 * k_u \text{ average} = 0.5 * 7.15 = 3.57$

- and for PI controller :

$$k_{c2} = 0.45 * k_u \text{ average} = 0.45 * 7.15 = 3.22 \text{ and } \tau_I = P_u \text{ average} / 1.2 = 4.08 / 1.2 = 3.4$$

- for PID controller :

$$k_{c2} = 0.6 * k_u \text{ average} = 0.6 * 7.15 = 4.29 \text{ and } \tau_I = P_u \text{ average} / 2 = 4.08 / 2 = 2.04, \tau_D = P_u \text{ average} / 8 = 4.08 / 8 = 0.51$$

The response of the system after tuning:

MATLAB is used to plot the step response from the closed loop transfer function:

The closed-loop transfer function:

$G(s)$

$$\frac{20.268k_{c1}}{= 2.45s + 18.254 + 36.453 + 79.4752 + 72.54s + 13.67 + 10.134k_{c1}}$$

step response for P control

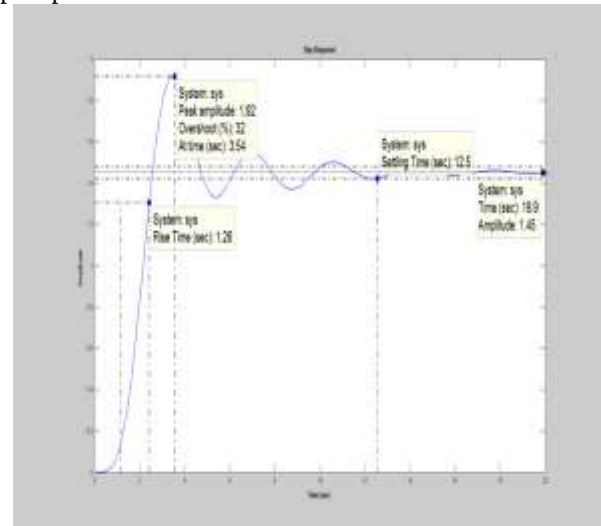


Fig 6: step response for P control

Step response for PI controller :

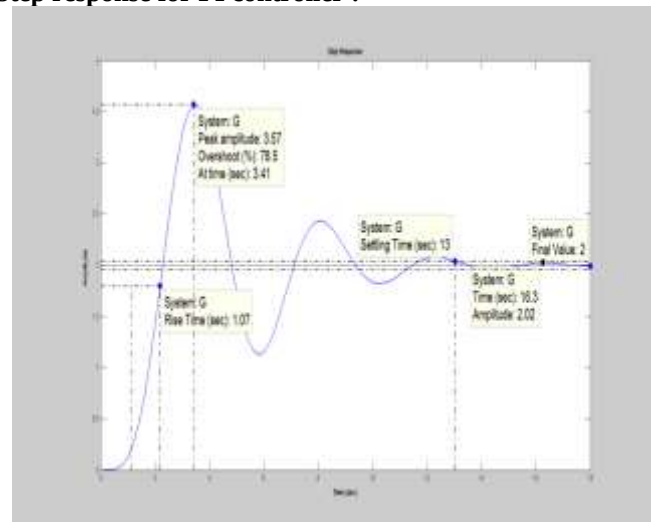


Fig7: step response for PI control

Step response for PI controller :

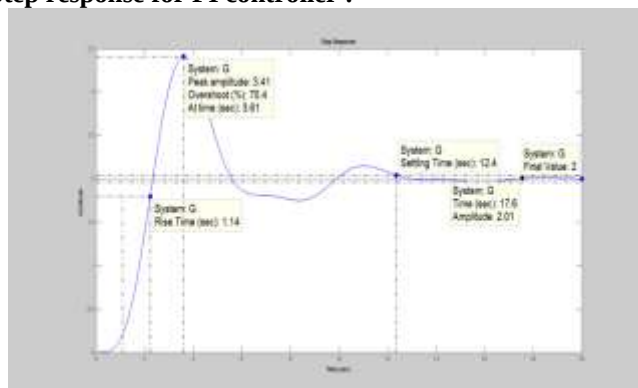


Fig 8: step response for PID control

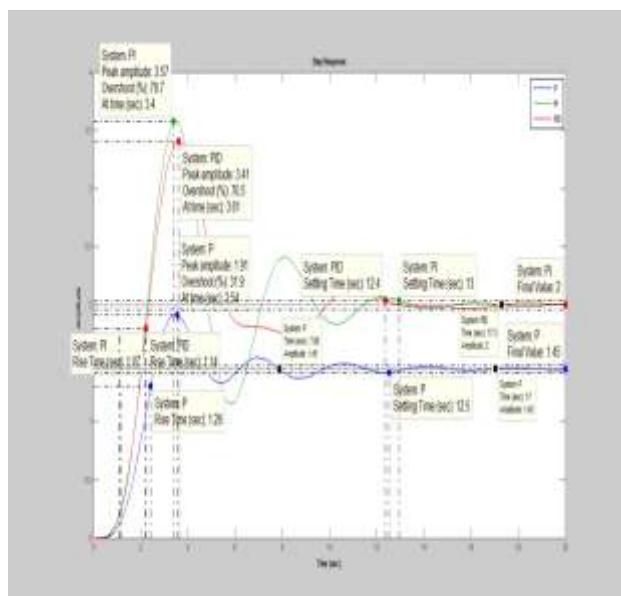


Fig 9: System step response for three type of controller

Table 1: comparisons of the three types of controllers:

	P	PI	PID
RiseTime sec	1.26	1.07	1.14
SettlingTime sec	12.5	13.0	12.4
SettlingMax sec	19.9	16.3	17.6
Overshoot%	31.9	78.7	70.5
@ time sec	@ 3.54	@ 3.41	@ 3.61
Peak amplitude	1.91	3.57	3.41

The selected controller for the primary loop from above table is P (min overshoot)

IV CONCLUSIONS:

A control strategy was devolved , the transfer functions were identified from the literature ,then the block diagram was

constructed and used to determine the ultimate gains and periods from which the adjustable parameters (K_c , τ_i , τ_d) were obtained and used for simulation , determination of the minimum overshoot and the controller that gave the minimum overshoot was selected and introduced in each loop (primary and secondary). These data were used for the top of the column as the bottom loops is to be treated similary. The stability and tuning methods are compared with each other and it is found that they are in agreement .It is observed that the responses of the system are stable with reasonable rise time, overshoot, undershoot, decay ratio and settling time.

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