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TECHNOLOGY, DEVELOPMENT STATUS AND APPLICATIONS OF THE SHORT PULSES GYROTRON TRAVELING -WAVE-TUBE

Vinay Kumar

Electronics and Communication Engineering Department,
Institute of Engineering and Technology, Lucknow, India

Abstract— The gyrotron traveling-wave tube amplifier (gyro-TWT) is mainly used as high power millimeter wave sources that addresses the well-known concept of the electron cyclotron maser (ECM) instability. This paper present technology, development status and application of the short pulses Gyro-TWT amplifiers over a long period of time. Mainly focused on the techniques, beam wave interaction structure, controlling instability, broadband operation, high-power, low magnetic field.

Keywords— high-order harmonic interaction, high-order mode interaction, bandwidth extending or broadband operation, waveguide wall loss. Electron cyclotron maser; gyrotron traveling-wave tube amplifier (gyro-TWT).

I. INTRODUCTION

Unlike linear beam tubes, gyro-devices employ an electron beam that consists of electronically accelerating electrons and the free energy remains in motion transverse in the applied magnetic field. In these devices, cyclotron resonances; (a new dimension in the interaction mechanism), permitting wave generation in simple and large-size as well as structures provides the physics underpinning. When the interaction involves the gyration motion of electrons in a static magnetic field, the synchronism condition can be written as $\omega - k_z v_z - s\Omega_c \cong 0$ (1) Where, ($s = 1, 2, \dots$) ω , k_z , v_z are the wave frequency, propagation constant and electron axial velocity respectively, ($k_z v_z = \text{doppler term}$) and s , Ω_c are the cyclotron harmonic number, and relativistic electron cyclotron frequency respectively. From equation (1) permits a simple fast-wave ($\omega/k_z > c$) interaction structure.

In electron cyclotron masers electromagnetic energy is emitted by relativistic electrons rotating in an outward longitudinal magnetic field. In ECMs, the effective frequency Ω_c corresponds to the relativistic electron cyclotron frequency:

$$\Omega_c = \Omega_{c0}/\gamma \text{ with } \Omega_{c0} = eB_0/m_0 \quad (2)$$

$$\text{and } \gamma = \left[1 - \left(\frac{v}{c}\right)^2\right]^{-\frac{1}{2}} \approx 1 + \frac{eV_0}{m_0 c^2} = 1 + \frac{eV_0}{511} \quad (3)$$

Where γ is the relativistic Lorentz factor, m_0 is the mass of an electron, e is the charge and V_0 , B_0 are the acceleration voltage in kV, magnitude of the guide magnetic field respectively.

The commercially available (the word record parameters) of maximum pulse is 140 GHz, 0.92 Mega-Watt-class gyrotrons using artificial diamond output power windows at 30 minutes pulse duration, 44% efficiency and 97.5% Gaussian mode purity. (CPI and European KIT-CRPP-TED (The Research University in the Helmholtz Association) collaboration). Employing a SDC (single-stage depressed collector) for energy recovery.

The JAEA-TOSHIBA 110 GHz gyrotron generated a 1.5 MW output power (maximum) in 4.0 second pulse duration at 45% efficiency.

The maximum energy of 2.88 GJ (word record) in 60 minutes at 0.8 Mega-Watt was generated with the Japan 170 GHz ITER gyrotron, also achieved 1 Mega-Watt, 800 second pulse duration at 55% efficiency and the output power of greater than 0.5 MW with the 57% efficiency record for tubes.

The Russian 170 GHz ITER gyrotron generated 0.99 Mega-Watt with a 1000 second pulse duration at 53 % efficiency and also achieved 1.2 Mega-Watt with a 100 second pulse duration and 53 % efficiency.

European 170 GHz coaxial-cavity gyrotron (prototype tube) achieved of the 2 MW, in short pulses, 96% Gaussian mode purity and 46% efficiency.

Numerous short-pulse applications, pulsed magnet with gyrotron achieved at frequencies up to 670 GHz deliver 210 kilo-Watt in 20 second at 20% efficiency, 1 THz deliver 5.3 kilo-Watt in at 6.1% efficiency and 1.3 THz deliver 0.5 kilo-Watt in 20 second at 0.6 % efficiency.

In this paper section II gave the details review of technologies for experimental design of gyro-traveling wave tube amplifier. In section III shows the status of present development of gyro TWT in table form. In section IV conclusion and future of gyro-TWT and section V gives references.

II. TECHNOLOGIES FOR EXPERIMENTAL DESIGN OF GYRO-TWT

In the prior gyro-TWT setups several types of interaction mechanism were applied Chu KR et al (2002, 2004). Each one setup discovered explanation to the problem to the of positive aspect. During these experiments time explore the key technology to developed and evaluate of the amplifier. For

better appreciate these technologies, make known to the problems introduce four characteristics, including 4 types of technology

- A. high-order harmonic interaction,
- B. high-order mode interaction,
- C. bandwidth extending or broadband operation,
- D. waveguide wall loss.

A. High-order harmonic interaction:

Developing and design of an experimental gyro TWT amplifier of a high-order harmonic is of great significance [Chu et al (2004)].

1. The harmonic number is inversely proportional to the magnetic field strength; Hence, the magnetic field intensity is reduced by harmonic interaction. As an example, developing Ka-band gyrotron amplifier for the application of military. Necessitates about 0.6 Tesla magnetic field strength for second harmonic structure. While only about 1.2 Tesla magnetic field strength necessitates the fundamental harmonic structure, and the first choice is superconducting magnet. For reducing the cost and improving the reliability on a normal coil used gyrotron amplifier.
2. The fundamental interaction coupling strength is greater than the operating mode, that while improve the threshold current of the total instability. Therefore, the device achieves stronger wave radiation power and may work at higher current [Wang QS, 1995].
3. Cyclotron beams (Large-orbit) with electron controlling center $r_c = 0$ are recommended in a higher-order harmonic interaction structure. Thus, only for the modes with azimuthal index equaling to the cyclotron harmonic number, they have nonzero beam-wave coupling coefficient. Specifically, in a large-orbit interaction structure, TE_{mn} mode ($m = s$) can only successfully interact with the s harmonic mode.

University of California Los Angeles (UCLA) [Furno DS, 1990] and University of California Davies (UC Davies) [Wang QS et.al, 1996] launched the experiments on harmonic Gyro-TWT amplifier. In 1990, the UCLA perform an experiment on harmonic gyrotron amplifier, that operated in 8th harmonic. Circular waveguide and large orbit electron beam are used. The current, voltage and output power were 150 mA, 350 kV and 0.5 kW respectively. The efficiency of Ku band, gain and bandwidth were 1.35%, small signal 10 dB, and 4.3% respectively.

In 1996, UC Davies using second harmonic gyro-TWT interaction carried out an experiment. The interaction circuit as shown in figure 1 was design as; an axial sliced circular waveguide, and four slices with 90° interval along the axis.

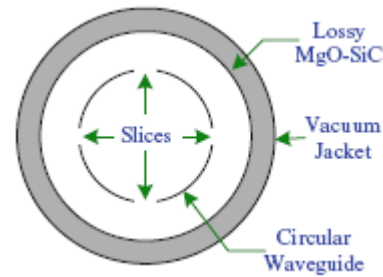


Figure 1: Sectional view of the sliced interaction waveguide.

In this special structure, TE_{n1} mode (n is odd) can be done efficiently the mode competition and scattered was also debilitated. The experiment structure utilized harmonic interaction and wall loss technology. The experiments effectively established that fundamental interactions were less threshold current than harmonic interactions.

In 1998, UC Davies, also carried out an experiment using third harmonic gyro-TWT interaction experiments structure, X-band operated. The circuit as shown in figure 2 was a slotted waveguide: for the purpose of mode selection at intervals of 60°, six slots in waveguide wall along the axis. There were at intervals of 120° also three slices that gave scattered loss. The device operating current and operating voltage are 8 A and 66 kV respectively in π mode with 1.05 velocity. Experimental device results show; 6 kW output power, 11 dB gain, 3% bandwidth and 5% efficiency.

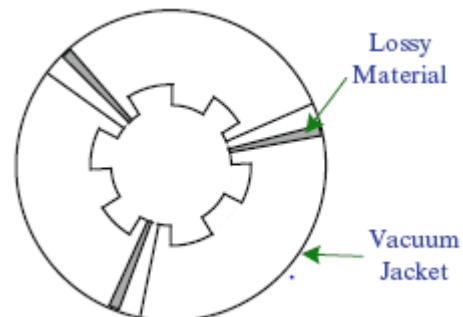


Figure 2: Sectional view of the slotted waveguide.

Theoretically we say that, a harmonic gyro-TWT provided higher output power and can operate on higher current. However, this is not always the result of the experiment. The magnetic field strength of the traditional system is several times greater than for harmonic operation. From lower-order harmonics, the mode competitions are unavoidable to encounter. Harmonic interaction system can be resolved all three issues of aspects:

1. To compress mode competition and to express the mode density through the suitable mode control mechanisms.
2. For improving the competing instability threshold current required to introduce appropriate lossy mechanism. Therefore, harmonic interaction systems were still very imperative subjects to resolve the mode competition and stability problem.



3. To enhance the interaction efficiency, to increase the beam-wave coupling strength to adopt high voltage.

B. High Order Mode Interaction Circuit:

In Millimeter-wave band and beyond wave band the higher-order-mode interaction operation is the key reason that vacuum electronic devices based on ECM principle are capable of achieving higher output power than conventional VEDs. A high order mode improves the power capacity and interaction space. Still now, gyro-TWT experiments have TE_{10} mode in rectangular waveguide [Park GS et al., 1995], TE_{01} mode in cylindrical waveguide [Pershing DE et al., and Nguyen KT et al., 2004, 2001], TE_{11} mode in cylindrical waveguide [Calame JP et al, and Garven M et al, 2002], TE_{21} mode in cylindrical waveguide [Wang QS et al, 1996], TE_{11}/TE_{21} mode in helical corrugated waveguide [Bratman et al, and Denisov GG, 2000, 1998], π mode in cylindrical waveguide with six azimuthal slots [Chong CK et al, 1998], and HE_{06} mode in confocal waveguide. In other word say that gyro- TWT amplifiers works on higher order mode interaction low order modes as compare to gyrotron oscillator. In a gyro-TWT experiment based on a confocal waveguide, MIT carried out on 140 GHz HE_{06} mode with open side walls.

C. Bandwidth Operation:

Developing of gyro-TWT in its initial stage proved the advantage of broadband. Rectangular TE_{10} mode waveguide gyro-TWT Ka-band tapered experiment was carried out [Park GS et al, 1994]; The output power and bandwidth were 6.3 kW and 33% respectively with 10% efficiency and 16.7 dB gain. In another a later experiment, drifting waveguide divided the single stage tapered circuit into a double stage tapered circuit in the section of under-cutoff, toward both ends external tapered. The system was increased stability; however, there was still possibility of oscillation [Park GS et al, 1995]. The double tapered circuit experiment carried out; 8 kW output power, 16% efficiency, 25 dB gain and 20% bandwidth. Even through the circuit increase the bandwidth.

University of California, Los Angeles (UCLA) in the middle of 1990s [Rao SJ et al, 1996], using dielectric-loaded rectangular waveguide, X-band gyro-TWT experiment carried out, output power and gain were 55 kW and 27 dB respectively with 11% bandwidth and efficiency. To improve results another more experiments done [Rao SJ et al (1996) , Cross AW (2007), Guo H et al, (1982)].

Cooperation with Russia Institute of Applied Physics (IAP) and University of Strathclyde, Glasgow, UK developed for broad band operation [Denisov GG et al, 1998] helical corrugated waveguide based gyro-TWT amplifier works on a coupled mode and is capable of broadband operation. Since 1998, helical corrugated waveguide based experiments are continue study by University of Strathclyde and IAP. Early experiment was X-Band based on second harmonic interaction

with 200 kV voltage and 25 A current it carried out 1MW output power, greater than 10% bandwidth ,23 dB gain and 20% efficiency. An improve experiments setup carried out output power, relative bandwidth and gain were 1.1 MW, 21% and 37 dB, respectively.

In 2002 another Ka-band experiment generate using voltage 80 kV and current 20 A (large orbit electron beam), it generates output peak power 180 kW, bandwidth 10% gain 27 dB and efficiency 27 %. In 2007 using a electron beam another X-band experiment of current 6 A and voltage 185 kV, it carried out output power 185 kW, bandwidth 2 GHz and gain 24 dB. Helical corrugated waveguide based gyro-TWT amplifier has advantages from two characteristics:

1. It operates on coupled mode; $k_z \approx 0$, with small propagation constant closed to region. Which makes it insensitive to the propagation of the electron beam.
2. The harmonic operation magnetic field strength is basically much lower than the conventional harmonic scheme.

D. Waveguide Wall Loss

Until now, the waveguide wall loss is the most successful solution to suppress the instability competition problem in gyro-TWTs. By loading a certain kind of wave dissipating material is realized the waveguide wall loss, during its propagation on the magnificent a distributed loss and waveguide wall consequence to wave mode, while find the negligible disturbance to the operating mode supply.

In American NRL early 1980s revealed a series of experiments in that the interaction circuits loaded with distributed waveguide wall loss were accomplished of increasing the stability and gain of a gyro-TWT [LauYY et al (1981,1982)]. To base on the distributed wall loss interaction circuit, firstly operated in Ka band gyro-TWT, mode interaction is TE_{01} with 3 A beam current, it carried out linear gain of 50 dB and pitch factor 1.5, [Barnett et al, 1980].

Prof. K. R. Chu and his group in 1990s [Chu Kr, et al, (1995, 1998, 1999, 2002, 2004)] based strong theoretical backup, achieved a series of Ka-band gyro-TWT experiments. In 1998, designed gyro-TWT experiment TE_{11} mode Ka band fundamental harmonic, it generates gain up to 70 dB (ultrahigh) output peak power 93 kW and efficiency 26.5 %. Noted that threshold current was improved 0.9A to 3.5 A.

In 1996 UCLA achieved Ku-band gyro-TWT as shown in figure 1. It operated at TE_{21} mode of second harmonic with pitch factor 1.1, current 20 A and electron beam voltage 80 kV. The experiment carried out peak power 207 kW, bandwidth 2.1%, gain 16 dB and efficiency 12.9%. From above waveguide wall loss technique review, it concluded that; in a gyro-TWT appreciate several ways :

- ❖ utilizing quasi-optical confocal waveguide with partial open boundary
- ❖ using ceramic-loaded cylindrical waveguide



- ❖ including lossy material filled sliced waveguide
- ❖ including coating lossy material on the inner wall of the waveguide
- ❖ using loading low conductivity material in the linear stage of the circuit

waveguide wall loss can be resolved all these issues are summarized as:

1. When the frequency becomes nearer to the cut-off frequency, then the wall loss inflicts to a mode much stronger attenuation, therefore occurs typically self-exciting oscillation.
2. The reflected wave in a lossy interaction system toward upstream end through the loss circuit travels inversely, so the downstream port has much stronger attenuation. Therefore, the driving power promises stable operation and the initial non-bunched cyclotron beam perform little influence in the input stage.

3. The wall-loss technique has the skill of suppressing the mode competition and selectively attenuation, and thus to suppress instability competition of gyro-TWTs can be usually applied the wall losses technique.

III. PRESENT DEVELOPMENT STATUS OF SHORT PULSE GYROTRON TRAVELING WAVE TUBE

The next generation of high-energy physics accelerators and the next frontier in understanding of elementary particles is based on supercolliders. Such generators are also required for atmospheric sensing and super-range high-resolution radar. Therefor Table 1 gives an overview of the present development status of short pulse relativistic gyrotron travelling wave tube (Gyro-TWT) amplifiers.

Table 1; Present Development Status of Short Pulse Relativistic Gyrotron Traveling Wave Tube.

Institution	Mode	Frequency (GHz)	Power (kw)	Bandwidth (%)	Gain (dB)	Efficiency (%)	Type
BVERI, Beijing [32-34]	TE_{01}	34.2	290 (5av.)	8.0	65	34	periodic SiC loading
	TE_{01}	48	150 (5av.)	7.0	50	35	periodic SiC loading
	TE_{01}	95	120	6.3	39	32	periodic SiC loading
CPI, Palo Alto [35-40]	TE_{11}	5.18	120	7.3	20	26	MIG
	TE_{11}	5.2	64	7.3	17.5	14	Pierce-helix gun
	TE_{11}	63.7	28	2	31	7.8	Pierce-helix gun
	TE_{01}	95	1.5 (0.6av.)	7.7	42	4.2	Pierce-helix gun
EEV, Chelmsford [41]	TE_{21}/TE_{+11}	10($2\Omega_e$)	180	--	--	--	gridded gun
IAP, Nizhny Novgorod [42-45]	TE_{21}/TE_{+11}	36.3($2\Omega_e$)	180	10	25	27	cusped gun with axis-encircle. Beam 3 μ s
	TE_{21}/TE_{+11}	34.3($2\Omega_e$)	120	6	20	23	long pulse 110 μ s
			160	1.3	27	36	250- μ s pulse (CW)
			7.7	7.5	27	33	
IECAS, Beijing [46-48]	TE_{11}	16.2	130	12.3	41	17.8	periodic lossy
	TE_{01}	34.5	110	5	33	15.2	periodic lossy
MIT, Cambridge [49-52]	HE_{01} (q.o.)	140	30	1.6	29	12.5	at 0.875 kW 400 ps modulation pulse PBG, 260 ps pulses
			.055	0.9	35	0.4	
	TE_{01} (like)	250	0.045	3.2	38	0.4	
NRL, Washington D.C. [53-54]	TE_{10}	32.5	6.3	33	16.7	10	1-stage tapered
	TE_{10}	35.5	8	20	25	16	2-stage tapered
	TE_{10}	32.3	50	11	25	28	folded waveguide axis-encircle Beam
	TE_{01}/TE_{11}	34.0	137	3.3	47	17	2-stage output
	TE_{01}/TE_{11}	35.6	70	17	60	17	2-stage output
UC Los Angeles / Davis [55-57]	TE_{10}	9.3	55	11	27	11	diel. coat. waveguide
	TE_{11}	10.4($3\Omega_e$)	6	3	11	5	axis-encircle. beam
	TE_{11}	15.7($2\Omega_e$)	207	2.1	16	12.9	slotted waveguide
	TE_{01}	16.2($8\Omega_e$)	0.5	4.3	10	1.3	axis-encircle. beam
	TE_{01}	92	140	2.2	60	22	heavily loaded + short copper stage
NTHU, Hsinchu [58-59]	TE_{11}	35.8	27	7.5	35	16	2-stage severed
	TE_{11}	34.2	62	12	33	21	2-stage lossy (short)
	TE_{11}	33.6	93	8.6	70	26.5	2-stage lossy (long)
UESTC, Chengdu [60-64]	TE_{11}	16	200 (20 av.)	16.3	43	23.8	3-stage lossy (long)
	TE_{01}	16	420	10	35	23	periodic lossy circuit
	TE_{01}	34	165 (11.5 av.)	10	45	27.5	lossy circuit
	TE_{01}	48	158	7	47	22.6	periodic lossy circuit



	TE_{01}	92.5	110	4.2	69.2	19.3	lossy circuit
University Kwangwoon [65]	TE_{10}	14.4	14.9	7	27	18	two-stage circuit
University Strathclyde [66-69]	TE_{-11}/TE_{+11}	93($2\Omega_e$)	3.4	5.8	37	4.2	cusp gun with axis-encircle beam
University Tel Aviv [70]	TE_{10}	7.3	0.8		26	12	3-stage output

IV. CONCLUSION

In this paper we have described technology issues and experimental setup or physics of the gyro-devices along with worldwide research highlights of these issues. An overview survey shows Gyro-TWT as a practical millimeter wave band and beyond one of the most promising devices of high-power generator, broadband operation, and high gain. It is revealed that gyro-TWT amplifiers are have mostly problems in developing of high power correlated to the uncertainty competition.

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